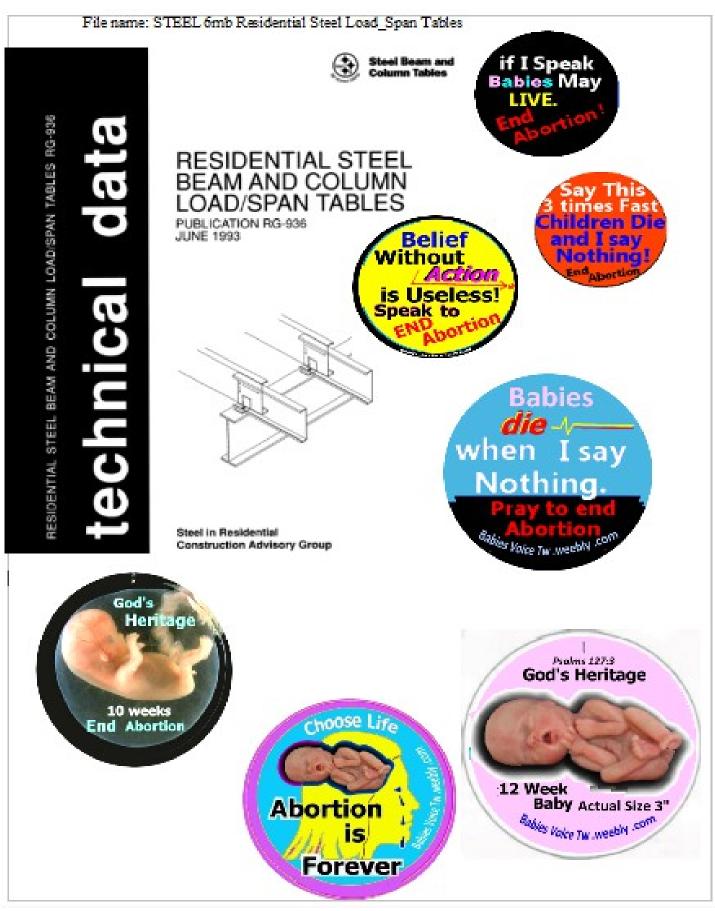
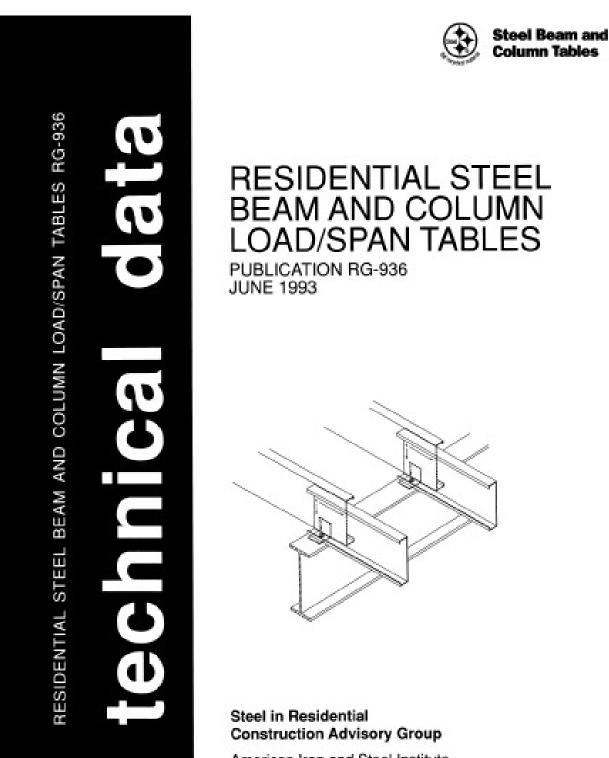
The "STEEL 12mb Residential Steel Load_Span Tables" Are here I just used some of the extraspace on each page to share some important information and websites. 2021July08How is your marriage?Do you apply God's Mercy?Bible Changes What does your bible remove??



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Residential Steel Beam and Column Load/Span Tables June 1993



ANGELS, What do they look like? Babies with wings? Beautiful Women? Men? Click here

INTRODUCTION

These tables were developed by the American Iron and Steel Institute with guidance from the AISI Residential Advisory Group. They are intended to provide designers and contractors with guidance on design of low-rise residential buildings that utilize steel structural members. AISI believes that the information contained in these tables substantially represents industry practice and related scientific and technical information, but the information is not intended to represent an official position of AISI or to restrict or exclude any other construction or design techniques. Additional design and detailing is required to incorporate these components into construction.

The American Institute of Steel Construction Specification for Structural Steel Buildings, dated June 1989 and Manual of Steel Construction, Allowable Stress Design, dated 1989 were used as the standards for the development of these tables. They are referenced throughout this publication and should be considered an integral part of structural steel design.

American Iron and Steel Institute June 1993

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Residential Steel Beam and Column Load/Span Tables

DISCUSSION

These load/span tables include beam and column sections that are commonly used in residential construction. The tables are based on information contained in the 1989 American Institute of Steel Construction (AISC), Allowable Stress Design, Specification and Manual and contain beams and columns supporting floor system spans or tributary widths ranging from 6 to 24 feet (in two foot increments).

A floor live load of 40 pounds per square foot (psf) on the first supported level and 30 psf on any additional levels was used in developing these tables for one, two and three supported floors. The tables include floor system dead loads of 10, 15 and 20 psf to account for various finishes or superimposed loads. The weight of the steel beams has been included in the calculations. In addition, the weight of the interior bearing wall supporting the second and third floors (as applicable) has been included. Roof system loads are not included. It is assumed that the roof system spans between exterior bearing walls. If the roof system is supported by the interior bearing walls and the roof loads do not exceed the floor loads used in the tables, the tables can be used assuming that the roof is considered an additional supported floor.

Beam Tables

Beam designs are based on single (simple) span conditions. This approach will provide some conservatism for multiple (continuous) spans. These spans are generally controlled by allowable moment capacities, but in some cases are limited so as not to exceed a live load deflection limit of L/360. In the case of continuous beams, spans limited by live load deflection will be somewhat conservative.

The tabulated beam span values are also based on a minimum of $1\frac{3}{4}$ inches of bearing along the axis of the beam at each beam end and $3\frac{1}{2}$ inches at each column where beams are continuous over the column. In some cases beam spans have been limited in order to

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maintain these bearing requirements. A bearing width perpendicular to the beam axis (in addition to the beam flange width) may also be required when the beam is supported on materials other than steel. Information on bearing plates and column cap and base plates is not included in the scope of these tables. Guidance on the design of beam and column bearings can be found in Part 2 and 3 of the AISC Manual.

Interpolation between values is not recommended since calculations are not linear. It is suggested that actual tributary widths be rounded-up to the next larger tabulated tributary width, when they fall between the tabulated dimensions. Beam spans should be measured from centerline (of bearing) to centerline of support. The top flange of beams must be laterally braced at a spacing less than or equal to the unbraced length (Lc) noted in the tables. To assure adequate bracing, members used to laterally brace the beam should be attached with fasteners that provide a positive connection.

Refer to Example 4 for guidance on the conversion of steel yield stresses for beams from 36 to 50 ksi. One of the advantages of 50 ksi steel is the added strength that is provided without the need to increase the beam size. This benefit is usually not as significant for spans controlled by deflection.

Column Tables

The column tables should not be used for the design of columns that change in section profile between the top plate and base plate, such as screw-jack or adjustable height columns. These columns are generally proprietary and require testing to establish load carrying capabilities. The manufacturer should be contacted for design capacities if these columns.

The column spacing dimensions listed in the column tables have been calculated assuming that the eccentricity of the total or resultant load is 1 inch or less from the column centerline. This eccentricity is provided to account for some moment induced into the column through minor eccentricities in beam bearing.



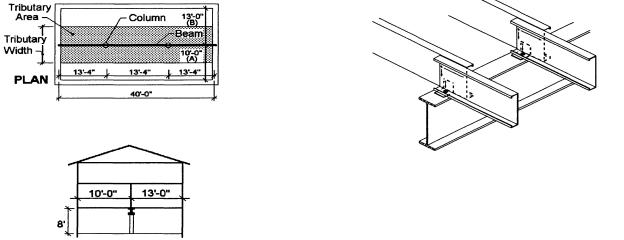
Eccentricities can exist as a result of connection detailing, unequal beam spans on each side of the column, and unequal (pattern) loads on each side of the column. These considerations occur most frequently with single span beam conditions and are demonstrated in Example 2. For continuous beams with concentric column bearing the tabulated values may be fairly conservative. Guidance on the design of columns with moments or eccentricities that are beyond the scope of these tables can be found in Part 3 of the AISC Manual.

The tables also assume that the columns are laterally braced at 8 feet above the slab on grade or base of the column, and should provide conservative results for columns less than 8 feet in height.

EXAMPLE 1

Determine the required center beam and column size for a two story house (two supported floors). See the plans for overall dimensions and spans. The local building code provisions require a floor live load of 40 pounds per square foot (psf) for dwelling units (except sleeping areas) and 30 psf for sleeping areas. The unbraced height of the column is 8 feet from the top of the slab-on-grade to the beam above. The roof is composed of single span trusses. The continuous beam applies concentric loads to the columns. Dead load (weight) of the floor system is as follows:

Floor Dead Load		Interior Bearing Wall Dead Load	<u>1</u>
Wood flooring	2.5	3-5/8" Steel Studs @ 24"x 8'	5.0
Subflooring	2.0	Top & Bot. Track	2.0
10" Steel Joists @ 24"	1.5	1/2" Gypsum Wallboard (ea. side) x 8'	<u>32.0</u>
1/2" Gypsum Wallboard Ceiling	2.0		39.0 plf
Misc. & Mech.	<u>2.0</u>		_
	10.0 psf		
	_		



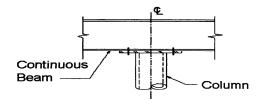
Solution: One continuous beam with two columns equally spaced is chosen. The top flange of the beam is to be braced at each joist (a positive connection is necessary between each joist and the beam). Provide a minimum of $1\frac{3}{4}$ inches of bearing at the beam ends and $3\frac{1}{2}$ inches of bearing at each column.

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Beam Design: Unbraced length = 2' < Lc: ok, joists are connected to the beam with anchor clips. Tributary width = (A+B)/2 = (13+10)/2 = 11'-6": Round up to 12'-0".
DL = 10 psf: Use the table on page 4.
DL wall < 50 plf: ok
L = 13'-4": Using the table on page 4, enter the column for the Tributary Width = 12'-0". Follow down the column until the values exceed 13.33 feet. A W8x18 or a W10x15 are the first beams that exceed the span requirements (14.5 and 13.8, respectively). If headroom is limited the W8x18 could be specified, but for greater economy the W10x15 will be used. USE W10x15

Check beam bearing plate requirements per the AISC Specification, since the ends will be supported on a concrete wall. Guidance on bearing design can be found on pages 2-31 and 2-141 through 2-144 of the 1989 AISC ASD Manual. Reactions may be determined as follows:



Simple beam loads = 13.33[11.5(10+10+40+30) + 39 + 15]= 14,516 lbs. Simple beam end reaction = (14,516)/2 = 7,258 lbs.

Adjust reactions to account for a continuous (one piece) beam. Using the coefficients on page 2-312 (3-span condition) of the AISC Manual:

> Continuous Beam Reaction at Exterior Supports = 14,516(4/10) = 5,806 lbs. Continuous Beam Reaction at Interior Supports = 14,516[(6+5)/10] = 15,968 lbs.

Column Design: Unbraced Length $\leq 8'$: ok

Tributary width = (A+B)/2 = (13+10)/2 = 11'-6": Round up to 12'-0". DL = 10 psf: Use the table on page 11. DL wall < 50 plf: ok L = 13'-4": Using the table on page 11, enter the column for the Tributary Width Supported by the Beam = 12'-0". Follow down the column until the values exceed 13.33 feet. This occurs with a 3" diameter Standard (STD.) pipe column (13.6 feet). USE 3" dia. STD. Pipe

Since the beam is continuous no further adjustments are necessary. The reactions calculated above for a continuous beam may be used to design for the cap and base plate requirements of the column. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual.

EXAMPLE 2

Use Example 1 except add a thick set tile floor to the system and use only one column. Increase the dead load to 20 psf to account for the tile flooring. The span of the beams is 20 feet.

Solution: Due to the possible weight of the steel beam and difficulties in handling during erection two single span beams will be used.

Beam Design: Unbraced length = 2' < Lc: ok (A+B)/2 = (13+10)/2 = 11'-6": Round up to 12'-0".
DL = 20 psf: Use the table on page 6.
DL wall < 50 plf: ok
L = 20'-0": Using the table on page 6, enter the column for the Tributary Width Supported by the Beam = 12'-0". Follow down the column until the values exceed 20.0 feet. A W14x26 is the first beam that equals the span requirements (20.0 feet). USE 2 ea. W14x26

load is 40 plf. The beams are to be continuous and adequate bearing will be provided. The continuous beams provide concentric loading on the columns.

Solution:

Beam Design: Unbraced length = 2' < Lc: ok (A+B)/2 = 34/2 = 17'-0": Round up to 18'-0". or use two rows of beams, 34/3 = 11'-4": Round up to 12'-0". DL = 15 psf: Use the table on page 5. DL wall < 50 plf: ok W8x15 for the 18'-0" floor span: From the table on page 5 the maximum span is 10.0 feet. W8x15 for the 12'-0" floor span: From the table on page 5 the maximum span is 12.2 feet.



Column Design: For the 18'-0" floor span and 10.0 foot beam span:

From the table on page 12 a 3.5" dia. STD. pipe column is ok (11.5 feet). For the 12'-0" floor span and 12.2 foot beam span: From the table on page 12 a 3" dia. STD. pipe column is ok (12.3 feet).

There are two options available. The first is to provide one beam line (17'-0" floor span) with three interior columns at 9 feet on center. The second option is to have two beam lines (11'-4" floor spans) with two rows of two interior columns at 12 feet on center. Although the first option utilizes less structural steel, the benefits of larger column spacings and shorter floor spans should be considered.

EXAMPLE 4

For greater economy utilize steel beams with a yield stress of 50 ksi for Example 1. Again, headroom is not a concern.

<u>Solution</u>: Since a W8x18 and a W10x15 meet the design criteria for Fy = 36 ksi, the first trial size for a 50 ksi steel will be a W8x15 and a W10x12 (by inspection the next smaller size will not work).

$L_{c-50} = L_{c-36}(36/50)$	For W8x15 $L_{c.50} = 4.2(36/50) = 3.0$ feet > 2 feet: ok
I (50/201/2	For W10x12 $L_{c.50} = 3.9(36/50) = 2.8$ feet > 2 feet: ok
$L_{50} = L_{36} (50/36)^{1/2}$	For W8x15 $L_{50} = 12.8(50/36)^{1/2} = 15.1$ feet: ok
	For W10x12 $L_{50} = 12.3(50/36)^{1/2} = 14.5$ feet: <i>ok</i>
Check Deflection	
$L_{LL-50} = L_{LL-36} / (S_R / S_{LL})^{1/3}$	L_{LL-36} = Maximum span where live load deflection first controlled the design (at any tributary width, (A+B)/2). $S_R = (A+B)/2$ required the actual case. $S_{LL} = (A+B)/2$ for the first case that is controlled by live load deflection.
	For W8x15 $L_{LL.50} = 15.4/(12/8)^{1/3} = 13.5$ feet < 15.0: Deflection controls, but it does exceed the required 13'-4" span. For W10x12, no $L_{LL.36}$ is tabulated: Calculate the deflection as follows:
	$\Delta_{LL} = 5wL^4/384(EI) \le L/360 = 13.33(12)/360 = 0.44"$ = 5[11.5(40+30)/1000](13.33) ⁴ (1728)/384(29000)(53.8) = 0.37" < 0.44": ok
Check bearing RE ₅₀ = RE ₃₆ $(50/36)^{1/2}$	
$RI_{50} = RI_{36}(50/36)^{1/2}$	Since the RE and RI values for the W10x12 are less than the values for the W8x15, check only the W10x12. See Example 1 for reactions. $RE_{50} = 11(50/36)^{1/2} = 12.96$ kips > 5,806 lbs or 5.8 kips: ok

 $RI_{50} = 29(50/36)^{1/2} = 34.18 \text{ kips} > 15,968 \text{ lbs or } 15.97 \text{ kips: } ok$

USE W10x12, Fy = 50 ksi





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 | 11.4 | LL | 10.9
 | ш | 10.6 | ш | 10.2 | Mc | 9.8 | 1
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14.7 14.</td></td></td> | B 23.4 4.2 20 42 20.4 9 21.6 3.9 11 29 21.2 2 30.1 5.5 18 40 22.2 8 27.3 4.2 17 38 23.0 2 36.0 5.6 21 45 23.7 2 32.1 4.2 18 41 24.4 9 41.4 6.9 21 46 24.5 9 29.5 3.5 12 30 25.0 8 37.2 4.2 20 45 25.7 3 48.1 6.9 28 55 25.9 1 33.9 4.1 14 36 26.3 2 45.9 6.1 18 41 27.6 3 42.2 4.2 17 40 28.5 9 55.2 6.1 22 49 29.4 4 5 | 8 23.4 4.2 20 42 20.4 LL 9 21.6 3.9 11 29 21.2 LL 2 30.1 5.5 18 40 22.2 LL 8 27.3 4.2 17 38 23.0 LL 2 30.1 5.5 18 40 22.2 LL 8 27.3 4.2 17 38 23.0 LL 2 36.0 5.6 21 45 23.7 LL 2 32.1 4.2 18 41 24.4 LL 9 41.4 6.9 21 46 24.5 LL 9 29.5 3.5 12 30 25.0 LL 9 29.5 3.5 12 30 25.7 LL 1 33.9 4.1 14 36 26.3 LL 2 45.9 6.1 18 41 27.6 LL 9 55.2 6.1 22 49< | 8 23.4 4.2 20 42 20.4 11 18.6 9 21.6 3.9 11 29 21.2 11 19.3 2 30.1 5.5 18 40 22.2 11 20.2 8 27.3 4.2 17 38 23.0 11 20.9 2 36.0 5.6 21 45 23.7 11 21.6 2 32.1 4.2 18 41 24.4 11 22.2 9 41.4 6.9 21 46 24.5 11 22.2 9 29.5 3.5 12 30 25.0 11 22.2 9 29.5 3.5 12 30 25.0 11 23.4 3 48.1 6.9 28 55 25.9 11 23.4 3 48.1 6.9 28 55 25.9 11 23.9 2 45.9 6.1 18 41 27.6 11 25.0 < | 8 23.4 4.2 20 42 20.4 11 18.6 11 9 21.6 3.9 11 29 21.2 11 19.3 11 2 30.1 5.5 18 40 22.2 11 20.2 11 2 30.1 5.5 18 40 22.2 11 20.2 11 2 30.1 5.5 18 40 22.2 11 20.9 11 2 36.0 5.6 21 45 23.7 11 21.6 11 2 36.0 5.6 21 45 23.7 11 22.2 11 9 41.4 6.9 21 46 24.5 11 22.2 11 9 29.5 3.5 12 30 25.0 11 22.2 11 9 29.5 3.5 12 30 25.0 11 23.4 11 13 38.1 6.9 28 55 25.9 11 23.5 | 8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 2 36.0 5.6 21 45 23.7 11 20.9 11 19.4 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 2 32.1 4.2 18 41 24.4 11 22.2 11 20.6 9 41.4 6.9 21 46 24.5 11 22.2 12 20.6 9 29.5 3.5 12 30 25.0 11 22.8 12 21.7 8 37.2 4.2 20 45 25.7 11 23.4 1 | 8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 11 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 11 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 11 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 11 2 32.1 4.2 18 41 24.4 11 22.2 11 20.6 11 9 29.5 3.5 12 30 25.0 11 22.8 11 11 11 8 37.2 4.2 20 45 25.7 11 23.4 11 21.7 11 | B 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 16.8 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 17.6 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 1 18.3 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 11 18.8 2 32.1 4.2 18 41 24.4 11 22.2 11 20.6 11 19.4 9 41.4 6.9 21 46 24.5 11 22.2 11 20.6 11 19.4 9 29.5 3.5 12 30 25.0 11 23.4 12.1.7 11 20.4 3 48.1 6.9 28 55 < | B 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 1 16.8 Me 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 17.6 11 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 11 18.3 11 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 11 18.8 11 2 32.1 4.2 18 41 24.4 11 22.2 11 20.0 11 18.8 11 2 32.1 4.2 18 41 24.4 11 22.2 11 20.6 11 19.4 11 9 29.5 3.5 12 30 25.0 11 21.7 11 20.4 </td <td>B 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 15.4 11 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 11 16.8 Mc 15.6 Mc 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 17.6 11 16.8 Mc 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 11 18.3 11 17.4 11 2 36.0 5.6 21 45 23.7 11 21.6 11 20.0 11 18.8 11 17.9 11 2 36.0 5.6 21 46 24.5 11 22.2 11 20.6 11 18.4 11 18.4 11 18.4 11 18.4 11 18.4 11 18.4 11 18.4 18.4 18.4 18.4</td> <td>8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 15.4 14.7 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 16.8 Mc 15.6 Mc 14.6 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 16.8 Mc 15.6 Mc 14.6 2 30.1 5.5 18 40 22.2 11 20.9 11 19.4 11.7.6 11.6.8 Mc 16.8 Mc 16.4 16.0 8 27.3 4.2 17 38 23.0 11 20.9 11 19.4 11.8.8 11 17.1
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 LL 20.2 LL 18.7 LL 17.6 LL 16.8 LL 16.0 LL 8 27.3 4.2 17 38 23.0 LL 20.9 LL 18.8 L 17.9 LL 16.4 Mc 2 36.0 5.6 21 45 23.7 LL 21.6 L 20.0 L 18.8 L 17.9 L 17.1 LL 2 32.1 4.2 18 41 24.4 L 22.2 L 20.7 L 19.4 L 18.5 L 17.7 LL 9 9 25.5 | B 23.4 4.2 20 42 20.4 LL 18.6 LL 17.2 LL 16.2 LL 15.4 LL 14.7 LL 14.2 9 21.6 3.9 11 29 21.2 LL 19.3 LL 17.9 LL 16.8 Mc 15.6 Mc 14.6 Mc 13.8 2 30.1 5.5 18 40 22.2 L 20.2 L 18.7 L 17.6 L 16.8 LL 16.0 L 15.4 8 27.3 4.2 17 38 23.0 L 20.9 L 18.7 L 16.8 L 16.0 L 15.4 8 27.3 4.2 18 41 24.4 L 22.2 L 20.0 L 18.8 L 17.9 L 17.1 L 16.7 16.7 9 41.4 6.9 21 46 24.5 L 22.2 L 20.7 L 19.4 L 18.5 | B 23.4 4.2 20 42 20.4 II 18.6 II 17.2 II 16.2 II 15.4 II 14.7 II 14.2 II 9 21.6 3.9 11 29 21.2 II 19.3 II 17.9 II 16.8 Mc 15.6 Mc 14.6 Mc 13.8 Mc 2 30.1 5.5 18 40 22.2 II 20.2 II 18.7 II 17.6 II 16.8 II 16.4 Mc 15.5 Mc 8 27.3 4.2 17 38 23.0 II 20.9 II 18.3 II 17.4 II 16.4 Mc 15.5 Mc 2 36.0 5.6 21 45 23.7 II 21.6 II 20.0 II 18.8 II 17.1 II 16.5 Mc 2 32.1 4.2 18 41 24.4 II 22.2 II 20.6 II | 8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 14.7 11 14.2 11 13.6 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 11 16.8 Mo 15.6 Mo 13.8 Mo 13.1 2 30.1 5.5 18 40 22.2 11 20.2 11 18.7 11 16.8 11 16.0 11 15.4 11 14.9 8 27.3 4.2 17 38 23.0 11 20.9 11 18.7 11 16.8 11 16.4 Mo 15.5 Mo 14.7 2 36.0 5.6 21 45 23.7 11 21.6 19.4 11 18.4 11 16.4 Mo 15.5 Mo 14.7 2 36.0 5.6 21 46 24.5 11 22.2 12.0 19.4 18.4 17.7 17.0 <td>8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 14.7 11 14.7 11 14.7 11 14.7 11 14.7 11 14.7 11 14.2 11 13.6 Mc 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 11 16.8 Mc 15.6 Mc 14.6 Mc 13.8 Mc 13.1 Mc 2 30.1 5.5 18 40 22.2 11 18.7 11 17.6 11 16.8 11 16.4 Mc 15.5 Mc 14.7 Mc 2 30.0 5.5 18 40 22.2 11 19.4 11 18.3 11 17.4 11 16.5 11 14.7 Mc 15.9 Mc 2 36.0 5.6 21 46 24.5 12.2 12.0 19.4 18.4 11.7.7 11.7.0 16.1 Mc 15.3<</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>A A A B B A A B B C A C B C <thc< th=""> <thc< th=""> <thc< th=""></thc<></thc<></thc<></td> <td>8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 15.4 11 14.7 11 14.2 11 13.6 Mc 12.4 Mc 12.4 13.6 Mc 12.4 14.7 14.</td> | 8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 14.7 11 14.7 11 14.7 11 14.7 11 14.7 11 14.7 11 14.2 11 13.6 Mc 9 21.6 3.9 11 29 21.2 11 19.3 11 17.9 11 16.8 Mc 15.6 Mc 14.6 Mc 13.8 Mc 13.1 Mc 2 30.1 5.5 18 40 22.2 11 18.7 11 17.6 11 16.8 11 16.4 Mc 15.5 Mc 14.7 Mc 2 30.0 5.5 18 40 22.2 11 19.4 11 18.3 11 17.4 11 16.5 11 14.7 Mc 15.9 Mc 2 36.0 5.6 21 46 24.5 12.2 12.0 19.4 18.4 11.7.7 11.7.0 16.1 Mc 15.3< | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | A A A B B A A B B C A C B C <thc< th=""> <thc< th=""> <thc< th=""></thc<></thc<></thc<> | 8 23.4 4.2 20 42 20.4 11 18.6 11 17.2 11 16.2 11 15.4 11 14.7 11 14.2 11 13.6 Mc 12.4 Mc 12.4 13.6 Mc 12.4 14.7
14.7 14.7 14. |



Pray to End Abortion





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1	MAXI	MUN	1 SPA	N FO			al Stee ER BE				•					-		roof	'or att	ic lo	oads) -	·L			(psf) ⁺ (psf)*	1: 4(
BEAN	I PROP	ERTIE	S (Min	1. Fy =	36ksi))					TR	IBUT	TARY	WID	TH SU	PPO	RTED	BY '	THE C	ENT	ER BE	AM ·	- (A+B)	/2		
SIZE	1	S	Mc	Lc	RE	RI	6'-0		8'-0		10'-()	12'-)	14'-(16'-()	18'-(20'-	0	22'-	0	24'-	-0
W6x9	16.4	5.6	11.0	4.2	11	26	14.3	LL	13.0	LL	12.0	LL	11.3	LL	10.6	Mc	10.0	Mc	9.4	Mc	8.9	Mc	8.5	Mc	8.1	M
W6x12	22.1	7.3	14.5	4.2	18	36	15.8	LL	14.3	LL	13.3	ш	12.5	ш	11.9	ш	11.4	LL	10.7	Mc	10.2	Mc	9.7	Мс	9.3	M
W8x10	30.8	7.8	15.5	4.2	10	26	17.6	LL	16.0	LL	14.9	ш	13.6	Mc	12.6	Mc	11.8	Mc	11 1	Mc	10.6	Mc	10.1	Mc	9.6	N
W6x16	32.1	10.2	20.2	4.3	22	45	17.9	ш	16.2	LL	15.1	ш	14.2	ш	13.5	LL	12.9	ш	12.4	ш	12.0	ш	11.5	Mc	11.0	N
W8x13	39.6	9.9	19.6	4.2	18	38	19.2	LL	174	LL	16.2	ш	15.2	LL	14.2	Mc	13.3	Mc	12.5	Mc	11.9	Mc	11.3	Mc	10.9	N
W8x15	48.0	11.8	23.4	4.2	20	42	20.4	LL	18.6	LL	17.2	LL	16.2	LL	15.4	LL	14.5	Mo	13.6	Mc	12.9	Mc	12.4	Mc	11.8	M
W10x12	53.8	10.9	21.6	3.9	11	29	21.2	LL	19.3	LL	17.5	Mc	16.0	Mc	14.9	Mc	13.9	Mc	13.1	Mc	12.5	Mc	11.9	Mc	11.4	N
W8x18	61.9	15.2	30.1	5.5	18	40	22.2	LL	20.2	LL	18.7	u	17.6	LL	16.8	Ш	16.0	11	15.4	LL	14.7	Mc	14.0	Mc	13.4	N
W10x15	68.9	13.8	27.3	4.2	17	38	23.0	LL	20.9	LL	19.4	ш	18.0	Mc	16.7	Mc	15.6	Mc	14.7	Mc	14.0	Mc	13.4	Mc	12.8	N
W8x21	75.3	18.2	36.0	5.6	21	45	23.7	LL	21.6	ш	20.0	LL	18.8	LL	17.9	LL	17.1	LL	16.5	LL	15.9	LL	15.3	Mc	14.7	N
W10x17	81.9	16.2	32.1	4.2	18	41	24.4	LL	22.2	ш	20.6	ш	19.4	LL	18.1	Mc	16.9	Mc	16.0	Mc	15.2	Mc	14.5	Mc	13.9	N
W8x24	82.8	20.9	41.4	6.9	21	46	24.5	LL	22.2	ш	20.7	LL	19.4	u	18.5	ш	17.7	LL	17.0	LL	16.4	LL	15.9	ш	15.4	
W12x14	88.6	14.9	29.5	3.5	12	30	25.0	LL	22.8	ш	20.5	Mc	18.7	Mc	17.4	Mc	16.2	Mc	15.3	Mc	14.6	Mc	13.9	Mc	13.3	N
W10x19	96.3	18.8	37.2	4.2	20	45	25.7	LL	23.4	LL	21.7	LL	20.4	ш	19.4	LL	18.2	Mc	17.2	Mc	16.3	Mc	15.6	Mc	14.9	N
W8x28	98.0	24.3	48.1	6.9	28	55	25.9	LL	23.5	ш	21.8	LL	20.6	LL	19.5	LL	18.7	LL	18.0	LL	17.3	ш	16.8	ш	16.3	l
W12x16	103.0	17.1	33.9	4.1	14	36	26.3	LL	23.9	ш	21.9	Mc	20.0	Mo	18.6	Mc	17.4	Mc	16.4	Mc	15.6	Mc	14.9	Mc	14.2	N
W10x22	118.0	23.2	45.9	6.1	18	41	27.6	LL	25.0					LL		ш										N
W12x19	130.0	21.3	42.2	4.2	17	40	28.5	LL	25.9					Mc		Mc										N
W10x26	144.0	27.9	55.2	6.1	22	49																				N
W12x22	156.0	25.4	50.3	4.3	21	49																				N
W10x30	170.0	32.4	64.2	6.1	29	58	31 1	LL						ш		ш				11						N
W14x22	199.0	29.0	57.4													Mc				Mo						N
																11										N
W12x19 W10x26 W12x22	130.0 144.0 156.0 170.0 199.0 245.0 m center of Inertia ble mom um unbra eam end	21.3 27.9 25.4 32.4 29.0 35.3 to cent , in. ⁴ ent assu- reactio	42.2 55.2 50.3 64.2 57.4 69.9 er of sup S = Els uming F ogth of ti n for 1-3	4.2 6.1 4.3 6.1 5.3 5.3 5.3 pports, astic Se b = 0. he beal 8/4" be	17 22 21 29 16 20 .ft. L m ection N 66Fy in m in or	40 49 58 37 46 hust be Accord der to u	28.5 29.4 30.2 31 1 32.8 35.1 > = dime s, in. ³ dance with use this tai	LL LL LL LL LL nnsion Men the ble a	25.9 26.8 27.5 28.3 29.8 31.9 n C, D, or mber Pro 1989 AIS nd Mc, ft s beam m	pertie CAS nax. r	es per the D Specifi eaction a	e 1989 ication	9 AISC A n, k-ft.	Mc LL LL Mc LL ngle s SD M	anual.				19.1 18.3 20.4 19.9 21.6 21.3 23.5 continou	Mc Mc LL Mc LL Mc s bes B		Mc Mc LL Mc LL Mc Mc e max sibutary butary butary			olumn	



What can I do about abortion? Thanks for being a voice for the children in the womb. I am grateful for whatever teaching you are doing to instruct people around you about the truth of abortion. We need to know and be aware of what is going on and being advocated on this topic. Over 23,000 babies are ripped out and trashed weekly in this country alone, and women are suffering the anguish of killing their own children. Mothers and the public as a whole are becoming more and more hardened to this atrocity as they search for ways of accepting the unspeakable actions they have already taken, not wanting to face the truth that abortion is a wickedness against God in killing his heritage.



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SIZE I W6x9 16.4	S			: 36ksi))				TR	IBU	TARY	WID	TH SU	PPO	RTED B	YТ	HE CI	ENT	ER BE	AM -	(A+B)	12		
W6x9 16.4		Mc	Lc	RE	RI	6'-0	8'-0		10'-0		12'-(14'-(16'-0	Т	18'-0		20'-4		22'-		24'-	0
the second se	5.6	11.0	4.2	11	26	14.3 LL	13.0	ш	12.0	Mc	11.0	Mc	10.2	Mc		Ac	9.0	Mc	8.5	Mc	8.1	Mc	7.8	M
W6x12 22.1	7.3	14.5	4.2	18	36	15.8 ц	14.3	LL	13.3	ш	12.5	ш	11.7	Mc		-	10.3	Mc	9.8	Mc	9.3	Mc	8.9	N
W8x10 30.8	7.8	15.5	4.2	10	26	17.6 ц	15.9	Mc	14.2	Mc	13.0	Mc	12.1	Mc		-	10.7	Mc	10.1	Mc	9.6	Mc	9.2	1
W6x16 32.1	10.2	20.2	4.3	22	45	17.9 u	16.2	ш	15.1	ш	14.2	ш	13.5	ш	12.9	_	12.1	Mc	11.5	Mc	11.0	Mc	10.5	,
W8x13 39.6	9.9	19.6	4.2	18	38	19.2 ц	174	ш	16.0	Mc	14.6	Mc	13.6	Mc		-	12.0	Mc	11.4	Mc	10.9	Mc	10.4	N
W8x15 48.0	11.8	23.4	4.2	20	42	20.4 LL	18.6	ш	17.2	LL	15.9	Mc	14.8	Mc	13.8	-	13.1	Mc	12.4	Mc	11.8	Mc	11.3	N
W10x12 53.8	10.9	21.6	3.9	11	29	21.2 ц	18.7	Mc	16.8	Mc	15.4	Mc	14.2	Mc		-	12.6	Mc	11.9	Mc	114	Mc	10.9	N
W8x18 61.9	15.2	30.1	5.5	18	40	22.2 LL	20.2	ш	18.7	ш	17.6	ш	16.8	Mc		-	14.8	Mc	14.1	Mc	13.4	Mc	12.9	N
W10x15 68.9	13.8	27.3	4.2	17	38	23.0 ц	20.9	ш	18.9	Mc	17.2	Mc	16.0	Mc			14.1	Mc	13.4	Mc	12.8	Mc	12.3	N
W8x21 75.3	18.2	36.0	5.6	21	45	23.7 ц	21.6	ш	20.0	ш	18.8	u	17.9	ш			16.2	Mc	15.4	Mc	14.7	Mc	14.0	N
W10x17 81.9	16.2	32.1	4.2	18	41	24.4 ц	22.2	ш	20.4	Mc	18.7	Mc	17.3	Mc	16.2		15.3	Mc	14.5	Mc	13.9	Mc	13.3	N
W8x24 82.8	20.9	41.4	6.9	21	46	24.5 LL	22.2	ш	20.7	ш	19.4	u	18.5	LL	17.7		17.0	LL	16.4	LL	15.7	Mc	15.0	N
W12x14 88.6	14.9	29.5	3.5	12	30	25.0 LL	21.9	Mc	19.6	Mc	17.9	Mc	16.6	Mc			14.7	Mc	13.9	Mc	13.3	Mc	12.7	N
W10x19 96.3	18.8	37.2	4.2	20	45	25.7 LL	23.4	ш	21.7	LL	20.1	Mc	18.6	Mc		-	16.5	Mc	15.6	Mc	14.9	Mc	14.3	N
W8x28 98.0	24.3	48.1	6.9	28	55	25.9 LL	23.5	ш	21.8	LL	20.6	ш	19.5	LL			18.0	LL	17.3	LL	16.8	ш	16.2	N
W12x16 103.0	17.1	33.9	4.1	14	36	26.3 LL	23.4	Mc	21.0	Mc	19.2	Mc	17.8	Mc	16.7	Ac	15.7	Mc	14.9	Mc	14.2	Mc	13.6	N
W10x22 118.0	23.2	45.9	6.1	18	41	27.6 LL	25.0	ш	23.2	ш	21.9	ш	20.6	Mc		-	18.3	Mc	17.3	Mc	16.5	Mc	15.9	N
W12x19 130.0	21.3	42.2	4.2	17	40	28.5 LL	25.9	u	23.3	Мс	21.4	Mc	19.8	Mc			17.5	Mo	16.6	Mc	15.9	Mc	15.2	N
W10x26 144.0	27.9	55.2	6.1	22	49	29.4 LL	26.8	ш	24.8	ш	23.4	ш	22.2	LL		Ac	20.0	Mc	19.0	Mc	18.1	Mc	174	N
W12x22 156.0	25.4	50.3	4.3	21	49	30.2 LL	27.5	ш	25.4	Mc	23.3	Mc	21.6	Mc		Ac	19.1	Mc	18.1	Mc	17.3	Mc	16.6	N
W10x30 170.0	32.4	64.2	6.1	29	58	31.1 ц	28.3	LL	26.2	ш	24.7	ш	23.5	LL	22.4		21.5	Mc	20.4	Mc	19.5	Mc	18.7	N
N14x22 199.0	29.0	57.4	5.3	16	37	32.8 LL	29.8	LL	27.2	Mc	24.9	Mc	23.1	Mc	21.6	-	20.4	Mo	19.4	Mc	18.5	Mc	17.7	N
W14x26 245.0	35.3	69.9	5.3	20	46	35.1 LL	31.9	LL	29.6	ш	27 4	Mc	25.4	Mc	23.8	Ac	22.5	Mc	21.4	Mc	20.4	Mc	19.5	N

"180" has been called a half-hour of "video adrenaline," an "emotional rollercoaster," and "mind-blowing."

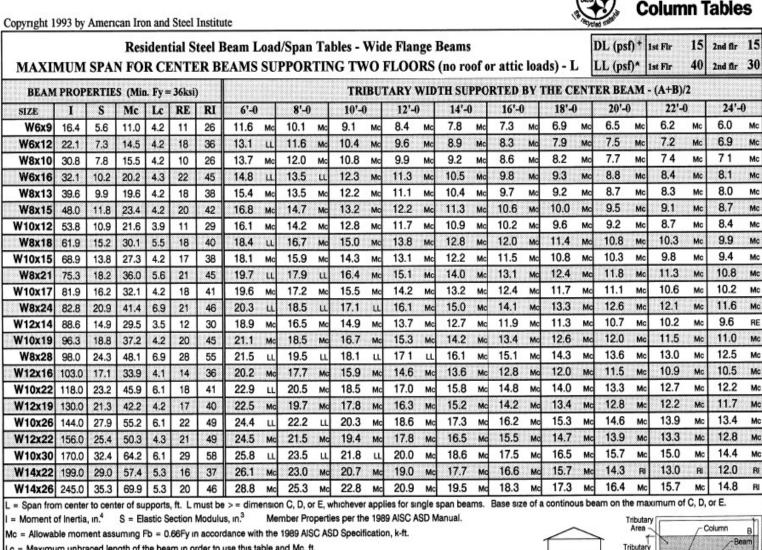


BEAM	PROP	ERTIE	S (Min	. Fy =	36ksi)	,			TRIBUT	ARY WID	TH SUPI	PO	RTED BY T	THE CE	10 I	nen	es			=
SIZE	I	S	Mc	Lc	RE	RI	6'-0	8'-0	10'-0	12'-0	14'-0	Т	16'-0	18'-0						The Length of this Page
W6x9	16.4	5.6	11.0	4.2	11	26	11.9 LL	10.6 Mc	9.6 Mc	8.8 Mc	8.2	Mc	7.7 Mc	7.2	1					9
W6x12	22.1	7.3	14.5	4.2	18	36	13.1 LL	11.9 u	11.0 мс	10.1 мс		Mc	8.8 Mc	8.3			100	1		
W8x10	30.8	7.8	15.5	4.2	10	26	14.4 мс	12.6 Mc	114 мс	10.4 мс		Mc	9.1 Mc	8.6		-	-			
W6x16	32.1	10.2	20.2	4.3	22	45	14.8 LL	13.5 LL	12.5 LL	11.8 ш	11.0	Mc	10.4 мс	9.8			-	-		
W8x13	39.6	9.9	19.6	4.2	18	38	15.9 LL	14.2 мс	12.8 Mc	11.7 мс	10.9	Mc	10.2 Mc	9.7			-	-		2
W8x15	48.0	11.8	23.4	4.2	20	42	16.9 LL	15.4 LL	13.9 мс	12.8 Mc		Mc	11.1 мс	10.5		-				
W10x12	53.8	10.9	21.6	3.9	11	29	16.9 мс	14.9 мс	13.4 мс	12.3 мс		Мс	10.7 мс	10.1						•
W8x18	61.9	15.2	30.1	5.5	18	40	18.4 LL	16.8 LL	15.6 LL	14.5 Mc		Mc	12.6 Mc	11.9						
W10x15	68.9	13.8	27.3	4.2	17	38	19.0 мс	16.7 мс	15.1 Mc	13.8 мс		Mc	12.1 Mc	11.4						
W8x21	75.3	18.2	36.0	5.6	21	45	19.7 ц	17.9 LL	16.6 LL	15.6 LL		Мс	13.8 мс	13.1		-	-			-
W10x17	81.9	16.2	32.1	4.2	18	41	20.2 LL	18.1 Mc	16.3 Mc	15.0 Mc		Mc	13.0 Mc	12.3	unbo	ical	aby a age <u>D</u>	it 20	wee	KS,
W8x24	82.8	20.9	41.4	6.9	21	46	20.3 LL	18.5 LL	17.1 LL	16.1 LL		ш	14.7 LL	14.0	D&E					
W12x14	88.6	14.9	29.5	3.5	12	30	19.8 мс	174 мс	15.6 Mc	14.4 Mc		Mc	12.5 Mc	11.8 M		MCI	10.7	Mc	10.3	M
W10x19	96.3	18.8	37.2	4.2	20	45	21.4 LL	19.4 LL	17.5 Mc	16.1 Mc		Mc	14.0 Mc	13.3 M		Mc	12.1	Mc	11.6	Mo
W8x28	98.0	24.3	48.1	6.9	28	55	21.5 LL	19.5 LL	18.1 LL	17.1 LL		LL	15.5 LL	14.9 ц	14.3	Mc	13.7	Mc	13.1	M
W12x16	103.0	17.1	33.9	4.1	14	36	21.1 мс	18.6 мс	16.7 мс	15.4 мс		Mc	13.4 мс	12.7 M		Mc	11.5	Mc	11.0	Mo
W10x22	118.0	23.2	45.9	6.1	18	41	22.9 LL	20.8 LL	19.3 LL	17.9 мс		Mc	15.6 мс	14.7 M		Mc	13.4	Mc	12.8	M
W12x19	130.0	21.3	42.2	4.2	17	40	23.5 мс	20.7 Mc	18.7 Mc	17.1 Mc		Mc	15.0 Mc	14.1 M		Mc	12.8	Mc	12.3	Mo
W10x26	144.0	27.9	55.2	6.1	22	49	24.4 LL	22.2 LL	20.6 LL	19.4 LL		Mc	171 Mc	16.1 M		Mc	14.7	Mc	14.1	Mo
W12x22	156.0	25.4	50.3	4.3	21	49	25.1 LL	22.5 Mc	20.3 Mc	18.7 Mc		Mc	16.3 Mc	15.4 M		Mc	14.0	Mc	13.4	Mo
W10x30	170.0	32.4	64.2	6.1	29	58	25.8 LL	23.5 LL	21.8 LL	20.5 LL		LL	18.4 мс	174 м		Mc	15.8	Mc	15.1	Mo
W14x22		29.0	57.4	5.3	16	37	27.2 LL	24.1 мс	21.7 мс	20.0 мс		Mc	17.4 Mc	16.5 M		Mc	14.4	RI	13.3	RI
W14x26		35.3		5.3	20	46	29.2 LL	26.5 LL	23.9 мс	22.0 Mc		Mc	19.2 Mc	18.2 M		Mc	16.5	Mc	15.8	M
= Moment o lc = Allowal c = Maximu E = Max. b No live load pan dimens reater bear	of Inertia ble mom im unbra eam end reduction sions are	, in. ⁴ ent ass aced len reactio ns have govern	S = Ela uming F igth of the n for 1-3 been in ed as no	astic Se b = 0. he bea 3/4" be cluded. bted by	ection M 66Fy in m in or aring, F v either	Modulus accord der to u aps. R mome	s, in. ³ Me dance with the use this table a l = Continuous + <i>DL is in add</i> nt capacity (Me as on non-stee	s beam max. r ition to beam w c), live load de I supports. Gu	eaction at inter veight & 50ptf for flection of L/3 idance on bea	AISC ASD M n, k-ft. For supports w for the intenor w 60 (LL), or inte ring design ca	anual. vith 3-1/2" valls. mor (RI) or n be found	' bea	uring, kips. erior (RE) bea		TI Nonents.	ributary Area ibutary ridth	c	Col ↓D Manual	umn Bee J E	-
4		1.02	Con R.				0.5	ESIDENT						:					ne 199	3
	TH	ER	E ai	re t	hou	san	<u>ds of b</u>	<u>abies r</u>	<u>ipped a</u>	<u>apart d</u>	<u>aily a</u>	an	<u>nd if th</u>	<u>ere is</u>	<u>no re</u>	esp	<u>ect f</u>	or li	<u>ife</u>	
<u>no</u> t	thing	g els	se m	ate	rs.	<u>Th</u>	<u>e babie</u>	es and i	nother	<u>s need</u>	our v	VO	ices an	d acti	<u>on.</u> 1	he	child	lren	you	<u>l</u>
					sav	e ai	e likely	to incl	ude you	r cousi	ns an	d	grandc	hildre	n.					
								1 and ma												
]	Plea	ase	tell	<u>me an</u>	<u>y other</u>	ideas y	you ma	y hav	ve	to add	l to th	is list	<u>t_</u>				
	<u>I w</u> a	<u>ould</u>					any end		-		-						er ei	nail	:	

Residential Steel Beam Load/Span Tables - Wide Flange Beams

Website: **<u>BabiesVoiceTw.weebly.com</u>**

phone: <u>865-242-7541</u>



Lc = Maximum unbraced length of the beam in order to use this table and Mc, ft.

RE = Max. beam end reaction for 1-3/4" bearing, kips. RI = Continuous beam max. reaction at interior supports with 3-1/2" bearing, kips. No live load reductions have been included.

+ DL is in addition to beam weight & 50plf for the interior walls.

Span dimensions are governed as noted by either moment capacity (Mc), live load deflection of L/360 (LL), or interior (RI) or exterior (RE) bearing requirements. Greater bearing dimensions are usually required for beams on non-steel supports. Guidance on bearing design can be found on pages 2-141 through 2-144 of the 1989 AISC ASD Manual.

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RESIDENTIAL STEEL FRAMING

June 1993

D

L E

Width -

PLAN

С

Steel Beam and

List of Differences between God's voice & Satan's voice

I am rejoicing that people are being informed. OK so now what? What actions are you encouraging individuals that they can themselves take to be an active voice for the unborn? What encouragement do you have as an instructor to help people to know what they could be doing to bring about a change of heart in this nation? Actions that encourage and give strength to mothers, to be protective of their own children, of the gift God has given them. Actions that help people to see the unborn as a blessing as God sees them and calls them a heritage and a reward.

	NUM	SPAN					EAMS		-					-	Beams (no ro		r attic	loa	ds) - I	. 8	DL (ps LL (ps	<u> </u>	lst Flr 1st Flr	20 40	2nd fir 2nd fir	
BEAM	PROP	ERTIE	S (Mir	n. Fy =	36ksi))					TR	BUI	ARY	WID	TH SUI	PPO	RTED	BY 1	THE C	ENT	ER BE	AM	- (A+B)/	2		
SIZE	1	S	Mc	Lc	RE	RI	6'-0		8'-0		10'-0)	12'-(14'-0		16'-0		18'-(20'-0)	22'-()	24'-	-0
W6x9	16.4	5.6	11.0	4.2	11	26	11.1	Mc	9.7	Mc	8.7	Mc	8.0	Мс	74	Мс	7.0	Мс	6.6	Mc	6.2	Mc	6.0	Мс	5.7	M
W6x12	22.1	7.3	14.5	4.2	18	36	12.7	Mc	11.1	Mc	10.0	Mc	9.2	Мс	8.5	Мс	8.0	Mc	7.5	Mc	7.2	M¢	6.8	Мс	6.5	N
W8x10	30.8	7.8	15.5	4.2	10	26	13.1	Mc	11.5	Mc	10.3	Mc	9.5	Mc	8.8	Mc	8.2	Mc	7.8	Mc	74	Mc	71	Мс	6.8	N
W6x16	32.1	10.2	20.2	4.3	22	45	14.8	ш	13.1	Mc	11.8	Mc	10.8	Mc	10.0	Mc	9.4	Mc	8.9	Mc	8.4	Mc	8.1	Мс	7.7	N
W8x13	39.6	9.9	19.6	4.2	18	38	14.7	Mc	12.9	Mc	11.6	Mc	10.7	Mc	9.9	Mc	9.3	Mc	8.8	Mc	8.3	Мс	8.0	Mc	7.6	N
W8x15	48.0	11.8	23.4	4.2	20	42	16.1	Mc	14.1	Mc	12.7	Mc	11.6	Мс	10.8	Mc	10.1	Mc	9.6	Mc	9.1	Мс	8.7	Mc	8.3	N
W10x12	53.8	10.9	21.6	3.9	11	29	15.5	Mc	13.5	Mc	12.2	Mo	11.2	Mc	10.4	Mc	9.7	Mc	9.2	Mc	8.7	Mc	8.3	Mc	8.0	N
W8x18	61.9	15.2	30.1	5.5	18	40	18.2	Mc	15.9	Мс	14.4	Mc	13.2	Mc	12.2	Mc	11.5	Mc	10.8	Mc	10.3	Mc	9.8	Мс	9.4	1
W10x15	68.9	13.8	27.3	4.2	17	38	174	Mc	15.2	Mc	13.7	Mc	12.6	Mc	11.7	Mc	10.9	Mc	10.3	Mc	9.8	Mc	9.4	Мс	9.0	1
W8x21	75.3	18.2	36.0	5.6	21	45	19.7	LL	17.4	Mc	15.7	Mc	14.4	Mc	13.4	Mc	12.5	Mc	11.9	Mc	11.3	Мс	10.8	Мс	10.3	I
W10x17	81.9	16.2	32.1	4.2	18	41	18.8	Mc	16.5	Mc	14.8	Mc	13.6	Mc	12.6	Mc	11.9	Mc	11.2	Mc	10.6	Мс	10.2	Mc	9.7	,
W8x24	82.8	20.9	41.4	6.9	21	46	20.3	LL	18.5	LL	16.8	Mc	15.4	Mc	14.3	Мс	13.4	Mc	12.7	Mc	12.1	Мс	11.5	Mc	11.0	,
W12x14	88.6	14.9	29.5	3.5	12	30	18.1	Mc	15.8	Mc	14.2	Mc	13.1	Mc	12.1	Mc	11.4	Mc	10.7	Mc	10.2	Mc	9.5	RE	8.8	I
W10x19	96.3	18.8	37.2	4.2	20	45	20.2	Mc	17.7	Mc	16.0	Mc	14.6	Mc	13.6	Mc	12.8	Mc	12.1	Mc	11.5	Mc	10.9	Mc	10.5	
W8x28	98.0	24.3	48.1	6.9	28	55	21.5	LL	19.5	LL	18.1	Mc	16.6	Mc	15.4	Mc	14.5	Mc	13.7	Mc	13.0	Mc	12.4	Mc	11.9	I
W12x16	103.0	17.1	33.9	4.1	14	36	19.3	Mc	16.9	Mc	15.2	Мс	14.0	Mc	13.0	Mc	12.2	Mc	11.5	Mc	10.9	Mc	10.4	Mc	10.0	1
W10x22	118.0	23.2	45.9	6.1	18	41	22.4	Mc	19.6	Mc	17.7	Mc	16.2	Mc	15.1	Mc	14.2	Mc	13.4	Mc	12.7	Mc	12.1	Mc	11.6	1
W12x19	130.0	21.3	42.2	4.2	17	40	21.5	Mc	18.9	Mc	17.0	Mc	15.6	Мс	14.5	Мс	13.6	Mc	12.8	Mc	12.2	Mc	11.6	Мс	11.2	I
W10x26		27.9	55.2	6.1	22	49	24.4	ш	21.5	Mc	19.4	Mc	17.8	Mc	16.5	Mc	15.5	Mc	14.7	Mc	13.9	Mc	13.3	Мс	12.8	1
W12x22	156.0	25.4	50.3	4.3	21	49	23.4	Mc	20.6	Mc	18.5	Mc	17.0	Mc	15.8	Mc	14.8	Mc	14.0	Mc	13.3	Mc	12.7	Мс	12.2	1
W10x30	170.0	32.4	64.2	6.1	29	58	25.8	LL	23.1	Mc	20.9	Mc	19.1	Mc	17.8	Mc	16.7	Mc	15.8	Mc	15.0	Mc	14.3	Mc	13.7	1
W14x22		29.0	57.4	5.3	16	37	25.1	Mc	22.0	Mc	19.8	Mc	18.2	Мо	16.9	Mc	15.8	Mc	14.4	BI	13.0	RI	11.9	RI	10.9	
W14x26		35.3	69.9	5.3	20	46	27.6	Mc	24.2	Mc	21.8	Mc	20.0	Mc	18.6	Mc	17.5	Mc	16.5	Mc	15.7	Mc	14.7	RI	13.5	

Span dimensions are governed as noted by either moment capacity (Mc), live load deflection of L/360 (LL), or interior (RI) or exterior (RE) bearing requirements.

Greater bearing dimensions are usually required for beams on non-steel supports. Guidance on bearing design can be found on pages 2-141 through 2-144 of the 1989 AISC ASD Manual.

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RESIDENTIAL STEEL FRAMING

June 1993

Steel Beam and

People can be encouraged to see the need that everyone should be doing something to speak out against these children being taken to death, as these children can do nothing to help themselves.

1. Something very easy to do is to wear a Button that speaks for the unborn children. This is <u>something that can be done every day</u> to speak to church members, strangers, cashiers, neighbors, friends, and family. If people would just wear a button and ask people, "Would you like a free pro-life button?", this is a very easy way to bring up about 23,000 helpless children being killed by abortion weekly.

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	SFAR	FOR				Beam L AMS S		-					~			or atti	ic lo	ads) -	- E	DL (ps LL (ps		1st Flr 1st Flr		2, 3 Flrs 2, 3 Flrs	
BEAM PRO	PERTI	ES (Mii	n. Fy =	36ksi)					TR	IBUI	CARY	WID	TH SU	PPO	RTED	BY 1	THE C	ENT	ER BE.	AM	- (A+B)/	2		
SIZE I	S	Mc	Lc	RE	RI	6'-0	Τ	8'-0		10'-()	12'-	0	14'-()	16'-0		18'-()	20'-()	22'-()	24'-	0
W6x9 16.4	5.6	11.0	4.2	11	26	10.0	Mc	8.8	Mc	7.9	Mc	7.3	Mc	6.8	Mc	6.3	Mc	6.0	Mc	5.7	Mc	5.4	Mc	5.2	M
W6x12 22.1	7.3	14.5	4.2	18	36	11.4	Mc	10.0	Mc	9.1	Мс	8.3	Mc	7.7	Mc	7.3	Mc	6.9	Mc	6.5	Mc	6.2	Mc	6.0	м
W8x10 30.8	3 7.8	15.5	4.2	10	26	11.8	Mc	10.4	Mc	9.4	Мс	8.6	Mc	8.0	Mc	7.5	Mc	71	Mc	6.8	Mc	6.5	Mc	6.0	R
W6x16 32.1	10.2	20.2	4.3	22	45	13.2	ш	11.8	Mc	10.7	Mc	9.8	Mc	9.1	Mc	8.6	Mc	8.1	Mc	7.7	Mc	7.4	Mc	7.1	м
W8x13 39.6	9.9	19.6	4.2	18	38	13.3	Mc	11.7	Mc	10.5	Mc	9.7	Mc	9.0	Mc	8.5	Mc	8.0	Mc	7.6	Mc	7.3	Mc	7.0	м
W8x15 48.0) 11.8	23.4	4.2	20	42	14.5	Mc	12.7	Mc	11.5	Mc	10.6	Mc	9.8	Mc	9.2	Mc	8.7	Mc	8.3	Mc	7.9	Мс	7.6	м
W10x12 53.8	10.9	21.6	3.9	11	29	13.9	Mc	12.2	Mc	11 1	Mc	10.2	Mc	9.5	Mc	8.9	Mc	8.4	Mc	8.0	Mc	7.6	RE	7.0	R
W8x18 61.9	15.2	30.1	5.5	18	40	16.4	Mc	14.4	Mc	13.0	Mc	12.0	Mc	11.1	Mc	10.5	Mc	9.9	Mc	9.4	Mc	9.0	Мс	8.6	M
W10x15 68.9	13.8	27.3	4.2	17	38	15.6	Mc	13.8	Mc	12.4	Mc	11.4	Mc	10.6	Mc	10.0	Mc	9.4	Mc	9.0	Mc	8.6	Mc	8.2	M
W8x21 75.3	3 18.2	36.0	5.6	21	45	17.5	LL	15.8	Mc	14.2	Mc	13.1	Mc	12.2	Mc	11.4	Mc	10.8	Mc	10.3	Mc	9.8	Mc	9.4	M
W10x17 81.9	16.2	32.1	4.2	18	41	16.9	Mc	14.9	Mc	13.5	Mc	12.4	Mc	11.5	Mc	10.8	Mc	10.2	Mc	9.7	Mc	9.3	Mc	8.9	M
W8x24 82.8	3 20.9	41.4	6.9	21	46	18.0	ш	16.4	ш	15.2	LL	14.0	Mc	13.0	Mc	12.3	Mc	11.6	Mc	11.0	Mc	10.5	Мс	10.1	M
W12x14 88.6	3 14.9	29.5	3.5	12	30	16.2	Mc	14.3	Mc	12.9	Mc	11.9	Mc	11.0	Mc	10.4	Mc	9.7	RE	8.7	RE	8.0	RE	7.3	R
W10x19 96.3	18.8	37.2	4.2	20	45	18.2	Mc	16.0	Mc	14.5	Mc	13.3	Mo	12.4	Mc	11.6	Mc	11.0	Mc	10.5	Mc	10.0	Мс	9.6	м
W8x28 98.0	24.3	48.1	6.9	28	55	19.1	ш	17.3	LL	16.1	LL	15.1	Mc	14.1	Mc	13.2	Mc	12.5	Mc	11.9	Mc	11.3	Mc	10.9	M
W12x16 103.	0 17.1	33.9	4.1	14	36	17.4	Mc	15.3	Mc	13.8	Mc	12.7	Mc	11.8	M	11.1	Mc	10.5	Mc	10.0	Mc	9.5	Mc	8.8	R
W10x22 118.	0 23.2	45.9	6.1	18	41	20.2	Mc	17.8	Mc	16.1	Mc	14.8	Mc	13.8	M	12.9	Mc	12.2	Mc	11.6	Mc	11.1	RI	10.2	R
W12x19 130.	0 21.3	42.2	4.2	17	40	19.4	Mc	17.1	Mc	15.4	Mc	14.2	Mc	13.2	M	12.4	Мс	11.7	Mc	11.1	Mc	10.6	Mc	9.9	R
W10x26 144.	0 27.9	55.2	6.1	22	49	21.7	ш	19.5	Mc	17.6	Mc	16.2	Mc	15.1	M	14.2	Mc	13.4	Mc	12.7	Mc	12.2	Mc	11.7	M
W12x22 156.	0 25.4	50.3	4.3	21	49	21.1	Mc	18.6	Mc	16.8	Mc	15.5	Mc	14.4	M	13.5	Mc	12.8	Mc	12.2	Mc	11.6	Mc	11.1	M
W10x30 170.	0 32.4	64.2	6.1	29	58	22.9	ш	20.8	LL	18.9	Mc	174	Mc	16.2	Ma	15.2	Mc	14.4	Mc	13.7	Mc	13.1	Mc	12.6	M
W14x22 199.	0 29.0	57.4	5.3	16	37	22.6	Mc	19.9	Mc	18.0	Mc	16.5	Mc	15.3	R	13.5	RI	12.0	RI	10.9	RI	9.9	RI	9.1	R
W14x26 245.	0 35.3	69.9	5.3	20	46	24.8	Mc	21.9	Mc	19.8	Mc	18.2	Mc	17.0	M	15.9	Mc	14.9	RI	13.5	RI	12.3	RI	11.3	B

RESIDENTIAL STEEL FRAMING

June 1993



Steel Beam and Column Tables



3. Talking to family, friends, and neighbors (every day to several times a month)

4. Do things to activate more people i.e. Give people buttons, Invite people to come and pray at abortion's door with you, encourage others to share on social media and/or write to newspaper.

5. You can cut out and paste or tape pictures of babies in the womb or aborted on your out going mail such as bills, bank transactions, orders, letters,... and write some pro-life message with them, or a lesser thing would be to stick such info. Inside each thing, but fewer people would see it this way.





Steel Beam and **Column Tables**

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						-

MAXIM	IUM S	SPAN					Beam I AMS S							-			or att	ic lo	ads) -	- B	DL (ps LL (ps		lst Flr lst Flr		2, 3 Firs 2, 3 Firs	
BEAM	I PROP	ERTIE	S (Mir	1. Fy =	- 36ksi)					TR	BUI	ARY	WID	TH SU	PPO	RTED	BY 1	THE C	ENT	ER BE	AM ·	· (A+B)	/2		
SIZE	I	S	Mc	Lc	RE	RI	6'-0	Τ	8'-0	T	10'-() [12'-	0	14'-()	16'-(18'-()	20'-)	22'-	0	24'-	-0
W6x9	16.4	5.6	11.0	4.2	11	26	9.5	Mc	8.3	Mc	7.5	Mc	6.9	Mc	6.4	Mc	6.0	Mc	5.7	Mc	5.4	Mc	5.2	Mc	5.0	M
W6x12	22.1	7.3	14.5	4.2	18	36	10.9	Mc	9.5	Mc	8.6	Mc	7.9	Mc	7.4	Mc	6.9	Mc	6.5	Mc	6.2	Мс	5.9	Mc	5.7	м
W8x10	30.8	7.8	15.5	4.2	10	26	11.2	Mc	9.9	Mc	8.9	Mc	8.2	Mc	7.6	Mc	71	Mc	6.7	Mc	6.4	Mc	5.9	RE	5.4	R
W6x16	32.1	10.2	20.2	4.3	22	45	12.8	Mc	11.3	Mc	10.2	Mc	9.3	Mc	8.7	Мс	8.1	Mc	7.7	Mc	7.3	Mc	7.0	Mc	6.7	м
W8x13	39.6	9.9	19.6	4.2	18	38	12.6	Mc	11.1	Mc	10.0	Mc	9.2	Mo	8.6	Mc	8.0	Mc	7.6	Mc	7.2	Mc	6.9	Mc	6.6	M
W8x15	48.0	11.8	23.4	4.2	20	42	13.8	Мс	12.1	Мс	10.9	Mc	10.0	Mc	9.3	Mc	8.8	Mc	8.3	Mc	7.9	Mc	7.5	Mc	7.2	м
W10x12	53.8	10.9	21.6	3.9	11	29	13.3	Mc	11.7	Mc	10.5	Mc	9.7	Mc	9.0	Mc	8.4	Mc	8.0	Mc	7.5	RE	6.8	RE	6.3	RE
W8x18	61.9	15.2	30.1	5.5	18	40	15.6	Мс	13.7	Mc	12.4	Mo	11.4	Mc	10.6	Мс	9.9	Mc	9.4	Mc	8.9	Mc	8.5	Mc	8.2	м
W10x15	68.9	13.8	27.3	4.2	17	38	14.9	Mc	13.1	Mc	11.8	Mc	10.9	Mo	10.1	Mc	9.5	Mc	9.0	Mc	8.5	Mc	8.1	Mc	7.8	M
W8x21	75.3	18.2	36.0	5.6	21	45	17.1	Mc	15.0	Mc	13.5	Mc	12.4	Mc	11.6	Mc	10.9	Mc	10.3	Mc	9.8	Mc	9.3	Мс	8.9	м
W10x17	81.9	16.2	32.1	4.2	18	41	16.1	Mc	14.2	Mc	12.8	Mc	11.8	Mc	10.9	Mc	10.3	Mc	9.7	Mc	9.2	Mc	8.8	Mc	8.4	M
W8x24	82.8	20.9	41.4	6.9	21	46	18.0	ш	16.1	Mc	14.5	Mc	13.3	Mc	12.4	Mc	11.6	Mc	11.0	Mc	10.5	Mc	10.0	Mc	9.6	м
W12x14	88.6	14.9	29.5	3.5	12	30	15.5	Mc	13.6	Mc	12.3	Mc	11.3	Mc	10.5	Mc	9.7	RE	8.7	RE	7.9	RE	7.2	RE	6.6	R
W10x19	96.3	18.8	37.2	4.2	20	45	17.4	Mc	15.3	Мс	13.8	Mc	12.7	Mc	11.8	Mc	11.0	Mc	10.4	Mc	9.9	Mc	9.5	Mc	9.1	м
W8x28	98.0	24.3	48.1	6.9	28	55	19.1	LL	17.3	Mc	15.6	Mc	14.4	Mc	13.4	Mc	12.5	Mc	11.9	Mc	11.3	Mc	10.8	Mc	10.3	M
W12x16	103.0	17.1	33.9	4.1	14	36	16.6	Мс	14.6	Мс	13.2	Mc	12.1	Mc	11.2	Мс	10.5	Mc	10.0	Mo	9.5	RJ	8.6	BI	7.9	A
W10x22	118.0	23.2	45.9	6.1	18	41	19.2	Mc	16.9	Mc	15.3	Mo	14.0	Mc	13.1	Mc	12.3	Mc	11.6	Mc	10.9	RI	10.0	RI	9.2	R
W12x19	130.0	21.3	42.2	4.2	17	40	18.5	Mc	16.2	Mc	14.7	Mc	13.5	Mc	12.5	Мс	11.8	Mc	11.1	Mc	10.6	Мс	9.7	RI	8.9	R
W10x26	144.0	27.9	55.2	6.1	22	49	21.1	Mc	18.5	Mc	16.7	Mc	15.4	Mc	14.3	Mc	13.4	Mc	12.7	Mc	12.1	Mc	11.5	Mc	10.8	R
W12x22	156.0	25.4	50.3	4.3	21	49	20.1	Mc	17.7	Mc	16.0	Mc	14.7	Mc	13.7	Мс	12.8	Mc	12.1	Mc	11.5	Mc	11.0	Mc	10.6	M
W10x30	170.0	32.4	64.2	6.1	29	58	22.7	Mc	19.9	Mc	18.0	Mc	16.6	Mc	15.4	Mc	14.5	Mc	13.7	Mc	13.0	Mc	12.4	Mc	11.9	M
W14x22	199.0	29.0	57.4	5.3	16	37	21.5	Мс	18.9	Mc	17.1	Mc	15.7	Mc	13.8	RI	12.1	RI	10.9	RI	9.8	RI	9.0	RI	8.2	R
W14x26	245.0	35.3	69.9	5.3	20	46	23.7	Mc	20.9	Mc	18.8	Mo	17.3	Mc	16.1	Mc	15.0	RI	13.4	RI	12.1	BI	11.1	BI	10.2	R

Mc = Allowable moment assuming Fb = 0.66Fy in accordance with the 1989 AISC ASD Specification, k-ft.

Lc = Maximum unbraced length of the beam in order to use this table and Mc, ft.

RE = Max. beam end reaction for 1-3/4" bearing, kips. RI = Continuous beam max. reaction at interior supports with 3-1/2" bearing, kips.

* No live load reductions have been included. + DL is in addition to beam weight & 100plf for the intenor walls.

PLAN Span dimensions are governed as noted by either moment capacity (Mc), live load deflection of L/360 (LL), or interior (RI) or exterior (RE) bearing requirements Greater bearing dimensions are usually required for beams on non-steel supports. Guidance on bearing design can be found on pages 2-141 through 2-144 of the 1989 AISC ASD Manual

Area

Tributa Width

E

BEAM P	UM S	SPAN					Beam L AMS S		•					~			or att	ic lo	ads) -		DL (ps LL (ps		1st Flr 1st Flr		2, 3 Firs 2, 3 Firs	
	PROP	ERTIE	S (Min	1. Fy =	36ksi	,					TR	BUI	TARY	WID	TH SU	PPO	RTED	BY 7	THE C	ENT	ER BE	AM	- (A+B)/	2		
SIZE	I	S	Mc	Lc	RE	RI	6'-0	Т	8'-0	Т	10'-(12'-(0	14'-()	16'-() [18'-0		20'-0)	22'-()	24'-	0
W6x9	16.4	5.6	11.0	4.2	11	26	9.1	Mc	8.0	Mo	7.2	Mc	6.6	Mc	6.1	Mc	5.7	Мс	5.4	Mc	5.2	Mc	4.9	Mc	4.7	N
W6x12 2	22.1	7.3	14.5	4.2	18	36	10.4	Mc	9.1	Mc	8.2	Mc	7.5	Mc	7.0	Mc	6.6	Мс	6.2	Mc	5.9	Мс	5.6	Мс	5.4	N
W8x10 3	30.8	7.8	15.5	4.2	10	26	10.8	Mc	9.4	Mo	8.5	Мс	7.8	Mc	7.3	Mc	6.8	Mc	6.4	Mc	5.9	RE	5.4	RE	4.9	R
W6x16 3	32.1	10.2	20.2	4.3	22	45	12.3	Mc	10.8	Mc	9.7	Mc	8.9	Mc	8.3	Mc	7.8	Mc	7.3	Mc	7.0	Mc	6.7	Mc	6.4	N
W8x13 3	39.6	9.9	19.6	4.2	18	38	12.1	Mc	10.6	Mc	9.6	Mc	8.8	Mc	8.2	Mc	7.7	Mc	7.2	Mc	6.9	Mc	6.6	Mc	6.3	N
W8x15	48.0	11.8	23.4	4.2	20	42	13.2	Мс	11.6	Mc	10.4	Mc	9.6	Mc	8.9	Mc	8.4	Mc	7.9	Mc	7.5	Mc	7.2	Mc	6.9	N
W10x12	53.8	10.9	21.6	3.9	11	29	12.7	Mc	111	Mo	10.0	Mc	9.2	Mc	8.6	Mc	8.0	Mc	7.5	RE	6.8	RE	6.2	RE	5.7	R
W8x18	61.9	15.2	30.1	5.5	18	40	14.9	Mc	13.1	Mc	11.8	Mc	10.9	Mc	10.1	Мс	9.5	Mc	9.0	Mc	8.5	Mc	8.1	Mc	7.8	N
W10x15	68.9	13.8	27.3	4.2	17	38	14.3	Mc	12.5	Mc	11.3	Mc	10.4	Mc	9.6	Mc	9.0	Мс	8.5	Mc	8.1	Mc	7.8	Mc	74	N
W8x21	75.3	18.2	36.0	5.6	21	45	16.3	Mc	14.3	Mc	12.9	Mc	11.9	Mc	11.1	Mc	10.4	Mc	9.8	Mc	9.3	Mc	8.9	Mc	8.5	N
W10x17	81.9	16.2	32.1	4.2	18	41	15.4	Mc	13.6	Mc	12.2	Mc	11.2	Mc	10.4	Mc	9.8	Mc	9.3	Mc	8.8	Mc	8.4	Mc	8.1	N
W8x24	82.8	20.9	41.4	6.9	21	46	17.5	Mc	15.4	Mc	13.9	Mc	12.7	Mc	11.8	Mc	11.1	Mc	10.5	Mc	10.0	Mc	9.5	Мс	9.1	N
W12x14	88.6	14.9	29.5	3.5	12	30	14.8	Mc	13.0	Mc	11.7	Mc	10.8	Мс	10.0	Mc	8.9	RE	7.9	RE	7.2	RE	6.5	RE	6.0	F
W10x19	96.3	18.8	37.2	4.2	20	45	16.6	Мс	14.6	Мс	13.2	Mc	12.1	Мс	11.2	Mc	10.5	Mc	10.0	Mc	9.5	Mc	9.0	Mc	8.7	M
W8x28 9	98.0	24.3	48.1	6.9	28	55	18.8	Mc	16.5	Мс	14.9	Mc	13.7	Mc	12.7	Mc	12.0	Mc	11.3	Mc	10.8	Mc	10.3	Mc	9.8	١
W12x16 1	103.0	17.1	33.9	4.1	14	36	15.9	Mc	13.9	Mc	12.6	Mc	11.5	Mc	10.7	Mc	10.1	Mc	9.5	Mc	8.6	RI	7.9	RI	7.2	1
W10x22 1	18.0	23.2	45.9	6.1	18	41	18.4	Mc	16.2	Mc	14.6	Mc	13.4	Mc	12.5	Мс	11.7	Mc	11.0	RI	10.0	RI	9.1	RI	8.3	
W12x19 1	130.0	21.3	42.2	4.2	17	40	17.7	Mc	15.5	Mo	14.0	Mc	12.9	Mc	12.0	Mc	11.2	Mc	10.6	Mc	9.7	RI	8.8	RI	8.1	I
W10x26 1	144.0	27.9	55.2	6.1	22	49	20.2	Mc	17.7	Mc	16.0	Mc	14.7	Mc	13.7	Mc	12.8	Mc	12.1	Mc	11.5	Mc	10.7	RI	9.8	1
W12x22 1	156.0	25.4	50.3	4.3	21	49	19.3	Mc	16.9	Mc	15.3	Mc	14.0	Mc	13.1	Mc	12.2	Mc	11.6	Mc	11.0	Mc	10.5	Мс	9.8	1
W10x30 1	170.0	32.4	64.2	6.1	29	58	21.7	Mc	19.1	Mc	17.2	Mc	15.8	Mc	14.7	Мс	13.8	Mc	13.1	Mc	12.4	Mc	11.9	Mc	11.4	N
W14x22 1	199.0	29.0	57.4	5.3	16	37	20.6	Mc	18.1	Mc	16.3	Mc	14.5	RI	12.6	RI	11.1	RI	9.9	RI	8.9	RI	8.1	RI	7.5	1
	245.0	35.3	69.9	5.3	20	46	22.7	Mc	19.9	Mc	18.0	Mc	16.5	Mc	15.4	Mc	13.7	RI	12.2	RI	11.0	RI	10.1	RI	9.2	1

Steel Beam and

A list of actions to be a voice for the children and their mothers

Please tell me any other ideas you may have to add to this list I would love to hear any encouragement that you have to share. tony walker email: tonywBabies@yahoo.com Website: BabiesVoiceTw.weebly.com phone: 865-242-7541

Do you believe in mercy? My website: <u>http://mercy.as4u.us/mercy.html</u> Talks about how to apply Gods mercy to yourself.

TO WHOM is God's MERCY applied ?

Does God's Mercy apply to you?

Who is God's MERCY to? : Deuteronomy 7:9 Know therefore that the LORD thy God he is God. the faithful God which keeps covenant and mercy with them that love him and keep his commandments to a thousand generations;

Nehemiah 1:5 And said. I beseech thee, O LORD God of heaven, the great and terrible God, that keeps covenant and mercy for them that love him and observe his commandments:

Psalm 25:10 All the paths of the LORD are mercy and truth unto such as keep his covenant and his testimonies.

Proverbs 28:13 He that covers his sins shall not prosper: but whoso confesses and forsakes them shall have mercy.



Steel Beam and **Column Tables**

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		Colum	n Properti	es			TRIBUT	ARY WID	TH SUPPO	ORTED B	Y THE CEN	TER BEAN	4 - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	35.0	30.0	25.2	21.7	19.1	17.0	15.3	14.0	12.8
TS 3x3x0.1875	6.87	46	2.02	17	35	35.0	32.5	27.3	23.5	20.7	18.4	16.6	15.2	13.9
3.5"dia. STD.	9.11	36	2.68	22	44	35.0	35.0	34.6	29.8	26.2	23.4	21.1	19.2	17.7
TS 3x3x0.2500	8.81	46	2.59	21	44	35.0	35.0	33.7	29.1	25.5	22.8	20.6	18.7	17.2
											DL (psf)+	15	LL (psf)* 4
COLUMN		Colum	n Propert	es			TRIBUT	ARY WID	TH SUPP	ORTED B	Y THE CEN	TER BEAN	M - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	33.8	27.3	23.0	19.8	174	15.5	14.0	12.7	11.7
TS 3x3x0.1875	6.87	46	2.02	17	35	35.0	29.6	24.9	21.4	18.8	16.8	15.2	13.8	12.7
3.5"dia. STD.	9.11	36	2.68	22	44	35.0	35.0	31.6	27.2	23.9	21.3	19.2	17.5	16.1
TS 3x3x0.2500	8.81	46	2.59	21	44	35.0	35.0	30.8	26.5	23.3	20.8	18.7	17.1	15.7
											DL (psf)+	20	LL	psf)* 4
COLUMN		Colum	n Propert	ies			TRIBUT	ARY WID	TH SUPP	ORTED B	Y THE CEN	TER BEAL	M - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	31.1	25.2	21.1	18.2	16.0	14.2	12.8	11.7	10.7
TS 3x3x0.1875	6.87	46	2.02	17	35	33.8	27.3	22.9	19.7	17.3	15.4	13.9	12.7	11.6
3.5"dia. STD.	9.11	36	2.68	22	44	35.0	34.6	29.0	25.0	22.0	19.6	17.7	16.1	14.8
TS 3x3x0.2500	8.81	46	2.59	21	44	35.0	33.7	28.3	24.4	21.4	19.1	17.2	15.7	14.4

RESIDENTIAL STEEL FRAMING

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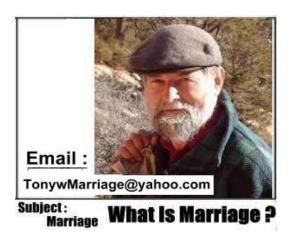
COLUMN		Colum	n Properti	ies			TRIBUT.	ARY WID	TH SUPPO	RTED BY	THE CEN	TER BEA	M - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	19.8	16.1	13.6	11.8	10.4	9.3	8.4	7.7	7.0
TS 3x3x0.1875	6.87	46	2.02	17	35	21.4	17.5	14.8	12.8	11.3	10.1	9.1	8.3	7.6
3.5"dia. STD.	9.11	36	2.68	22	44	27.2	22.2	18.7	16.2	14.3	12.8	11.5	10.5	9.7
TS 3x3x0.2500	8.81	46	2.59	21	44	26.5	21.6	18.2	15.8	13.9	12.4	11.2	10.3	9.4
3"dia. X-Strg.	10.25	36	3.02	20	45	25.7	20.9	17.7	15.3	13.5	12.0	10.9	9.9	9.1
TS 3x3x0.3125	10.58	46	3.11	24	51	30.3	24.7	20.8	18.0	15.9	14.2	12.8	11.7	10.8
4"dia. STD.	10.79	36	3.17	28	54	35.0	28.9	24.4	21 1	18.6	16.6	15.0	13.7	12.6
TS 4x4x0.1875	9.42	46	2.77	32	58	35.0	32.9	27.8	24.0	21.2	18.9	17.1	15.6	14.4
3.5"dia. X-Strg.	12.50	36	3.68	29	59	35.0	29.3	24.7	21.4	18.8	16.8	15.2	13.9	12.8
TS 4x4x0.2500	12.21	46	3.59	41	75	35.0	35.0	35.0	30.6	27.0	24.1	21.8	19. 9	18.3
4"dia. X-Strg.	14.98	36	4.41	38	75	35.0	35.0	33.2	28.7	25.3	22.6	20.5	18.7	17.2
3"dia. XX-Strg.	18.58	36	5.47	33	77	35.0	33.6	28.4	24.5	21.6	19.3	17.5	15.9	14.7
5"dia. STD.	14.62	36	4.30	45	78	35.0	35.0	35.0	33.7	29.7	26.5	24.0	21.9	20.1
TS 4x4x0.3125	14.83	46	4.36	48	90	35.0	35.0	35.0	35.0	31.8	28.4	25.7	23.4	21.6
Column loads are bas supported beams ma by = Minimum design = Gross cross-secti Pe = Maximum axial Pa = Allowable axial No live load reduction C+D)/2 has been lin	ny be single sp n yield stress p onal area of co load with an e load values fro ns have been i nited to 35 fee	ean or co per the A column per cocentrici om the 1 <i>included.</i> t to corre	ntinuous w ISC Specifi er the AISC ity of 1", pe 989 AISC - espond with	ith a max ication, k Manual, r the AIS ASD Max h the bea	amum ea si. K = in. C Manual nual, Allo + <i>DL i</i> s m tables	ccentricity of = 1.0 I, kips. wable Conce in addition to	1" for the res entric Load Ta beam weight	ultant load. ables, kıps. : & 50ptf for th	e interior wals	s.		Tributary Area Tributary Width	, °, °	lumn B Beam A
Column bearing desi	an must be pe	r the AIS	C Specific	ation. G	udance o	n base plate	design can l	be found on	pages 3-106 t	hrough 3-111	of the 1989 A	AISC ASD Ma	nual.	

What Is Marriage ? This Question has no meaning unless we base it on some authority. <u>What authority do you accept?</u>

Do You have a REAL Knowledge of Marriage? Who is family and how long do they remain family? Does divorce make those who were family, no longer family?

My people are destroyed for lack of knowledge:

because you have rejected knowledge, I will also reject you, that you shall be no priest to me: seeing you have forgotten the law of God, I will also forget your children. Hosea.4: 6







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MAXIMUM CO	DLUMN SP. TWO FLO									vhen C≠D;		L (psf) + L (psf)*	1st fir 15 1st fir 40	2nd flr 15 2nd flr 30
COLUMN		Column Properties TRIBUTARY WIDTH SUPPORTED BY THE CENTER BEAM - (A+B)/2												
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	18.0	14.6	12.3	10.7	9.4	8.4	7.6	6.9	6.4
TS 3x3x0.1875	6.87	46	2.02	17	35	19.5	15.9	13.4	11.6	10.2	9.1	8.2	7.5	6.9
3.5"dia. STD.	9.11	36	2.68	22	44	24.7	20.1	17.0	14.7	12.9	11.5	10.4	9.5	8.7
TS 3x3x0.2500	8.81	46	2.59	21	44	24.1	19.6	16.5	14.3	12.6	11.2	10.2	9.3	8.5
3"dia. X-Strg.	10.25	36	3.02	20	45	23.3	19.0	16.0	13.8	12.2	10.9	9.8	9.0	8.2
TS 3x3x0.3125	10.58	46	3.11	24	51	27.5	22.4	18.9	16.3	14.4	12.8	11.6	10.6	9.7
4"dia. STD.	10.79	36	3.17	28	54	32.2	26.2	22.1	19.1	16.8	15.0	13.6	12.4	114
TS 4x4x0.1875	9.42	46	2.77	32	58	35.0	29.8	25.2	21.8	19.2	17.1	15.5	14.1	13.0
3.5"dia. X-Strg.	12.50	36	3.68	29	59	32.6	26.5	22.4	19.3	17.0	15.2	13.7	12.5	11.5
TS 4x4x0.2500	12.21	46	3.59	41	75	35.0	35.0	32.0	27.7	24.4	21.8	19.7	17.9	16.5
4"dia. X-Strg.	14.98	36	4.41	38	75	35.0	35.0	30.1	26.0	22.9	20.5	18.5	16.9	15.5
3"dia. XX-Strg.	18.58	36	5.47	33	77	35.0	30.5	25.7	22.2	19.6	17.5	15.8	14.4	13.2
5"dia. STD.	14.62	36	4.30	45	78	35.0	35.0	35.0	30.5	26.8	24.0	21.7	19.8	18.2
TS 4x4x0.3125	14.83	46	4.36	48	90	35.0	35.0	35.0	32.7	28.8	25.7	23.2	21.2	19.5

Column loads are based on a maximum eccentricity of 1" between the resultant (total) load and the centerline of the colum

Supported beams may be single span or continuous with a maximum eccentricity of 1" for the resultant load.

Fy = Minimum design yield stress per the AISC Specification, ksi. K = 1.0

A = Gross cross-sectional area of column per the AISC Manual, in.

Pe = Maximum axial load with an eccentricity of 1*, per the AISC Manual, kips.

Pa = Allowable axial load values from the 1989 AISC - ASD Manual, Allowable Concentric Load Tables, kips.

* No live load reductions have been included.

(C+D)/2 has been limited to 35 feet to correspond with the beam tables.

Column bearing design must be per the AISC Specification. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual.

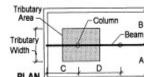
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RESIDENTIAL STEEL FRAMING

+ DL is in addition to beam weight & 50plf for the intenor walls.

June 1993





Lord help us to understand and obey your word and your will.

If we are not allowed to ask about any reason that brought about a divorce, we are forced to accept all reasons for all divorces.

When Paul says in Romans 7 and in 1Cor.7:39 "the woman... is bound by the law" Paul is talking about the law of Marriage from the creation. WHAT did Moses say???



Steel Beam and Column Tables

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COLUMN		Colum	n Propert	ies			TRIBUT	ARY WID	TH SUPPO	RTED BY	THE CEN	TER BEA	M - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	16.5	13.4	11.3	9.7	8.6	7.7	6.9	6.3	5.8
TS 3x3x0.1875	6.87	46	2.02	17	35	17.9	14.5	12.2	10.6	9.3	8.3	7.5	6.8	6.3
3.5"dia. STD.	9.11	36	2.68	22	44	22.7	18.4	15.5	13.4	11.8	10.5	9.5	8.7	8.0
TS 3x3x0.2500	8.81	46	2.59	21	44	22.1	17.9	15.1	13.0	11.5	10.3	9.3	8.4	7.8
3"dia. X-Strg.	10.25	36	3.02	20	45	21.4	174	14.6	12.6	11.1	9.9	9.0	8.2	7.5
TS 3x3x0.3125	10.58	46	3.11	24	51	25.2	20.5	17.2	14.9	13.1	11.7	10.6	9.6	8.9
4"dia. STD.	10.79	36	3.17	28	54	29.5	24.0	20.2	174	15.3	13.7	12.4	11.3	10.4
TS 4x4x0.1875	9.42	46	2.77	32	58	33.6	27.3	23.0	19.9	17.5	15.6	14.1	12.9	11.8
3.5"dia. X-Strg.	12.50	36	3.68	29	59	29.9	24.3	20.4	17.7	15.5	13.9	12.5	11.4	10.5
TS 4x4x0.2500	12.21	46	3.59	41	75	35.0	34.7	29.3	25.3	22.3	19.9	17.9	16.4	15.0
4"dia. X-Strg.	14.98	36	4.41	38	75	35.0	32.7	27.5	23.8	20.9	18.7	16.9	15.4	14.1
3"dia. XX-Strg.	18.58	36	5.47	33	77	34.3	27.9	23.5	20.3	17.8	15.9	14.4	13.1	12.1
5°dia. STD.	14.62	36	4.30	45	78	35.0	35.0	32.2	27.8	24.5	21.9	19.8	18.0	16.6
TS 4x4x0.3125	14.83	46	4.36	48	90	35.0	35.0	34.5	29.8	26.3	23.4	21.2	19.3	17.7

Pa = Allowable axial load values from the 1989 AISC - ASD Manual, Allowable Concentric Load Tables, kips.

* No live load reductions have been included. + DL is in addition to beam weight & 50plf for the interior wals.

(C+D)/2 has been limited to 35 feet to correspond with the beam tables.

Column bearing design must be per the AISC Specification. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual



RESIDENTIAL STEEL FRAMING

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MAXIMUM CO T	HREE FL								• • •	Second a second second se		L (psf) + L (psf)*	1st fir 10 1st fir 40	2&3 10 2&3 30
COLUMN		Column Properties TRIBUTARY WIDTH SUPPORTED BY THE CENTER BEAM - (A+B)/2												
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	13.5	11.0	9.3	8.1	71	6.4	5.8	5.3	
TS 3x3x0.1875	6.87	46	2.02	17	35	14.6	12.0	10.1	8.8	7.7	6.9	6.3	5.7	5.3
3.5"dia. STD.	9.11	36	2.68	22	44	18.6	15.2	12.8	111	9.8	8.8	7.9	7.2	6.7
TS 3x3x0.2500	8.81	46	2.59	21	44	18.1	14.8	12.5	10.8	9.6	8.5	7.7	7.1	6.5
3"dia. X-Strg.	10.25	36	3.02	20	45	17.5	14.3	12.1	10.5	9.3	8.3	7.5	6.8	6.3
TS 3x3x0.3125	10.58	46	3.11	24	51	20.7	16.9	14.3	12.4	10.9	9.8	8.8	8.1	7.4
4"dia. STD.	10.79	36	3.17	28	54	24.2	19.8	16.7	14.5	12.8	11 4	10.3	9.4	8.7
TS 4x4x0.1875	9.42	46	2.77	32	58	27.5	22.5	19.0	16.5	14.6	13.0	11.8	10.7	9.9
3.5"dia. X-Strg.	12.50	36	3.68	29	59	24.5	20.0	16.9	14.7	12.9	11.6	10.5	9.6	8.8
TS 4x4x0.2500	12.21	46	3.59	41	75	35.0	28.7	24.2	21.0	18.5	16.6	15.0	13.7	12.6
4"dia. X-Strg.	14.98	36	4.41	38	75	32.9	26.9	22.8	19.7	174	15.6	14.1	12.9	11.8
3"dia. XX-Strg.	18.58	36	5.47	33	77	28.1	23.0	19.4	16.8	14.9	13.3	12.0	11.0	10.1
5"dia. STD.	14.62	36	4.30	45	78	35.0	31.5	26.7	23.1	20.4	18.2	16.5	15.1	13.9
TS 4x4x0.3125	14.83	46	4.36	48	90	35.0	33.8	28.6	24.8	21.8	19.5	17.7	16.1	14.8

Supported beams may be single span or continuous with a maximum eccentricity of 1" for the resultant load.

Fy = Minimum design yield stress per the AISC Specification, ksi. K = 1.0

A = Gross cross-sectional area of column per the AISC Manual, in.

Pe = Maximum axial load with an eccentricity of 1", per the AISC Manual, kips.

Pa = Allowable axial load values from the 1989 AISC - ASD Manual, Allowable Concentric Load Tables, kips.

* No live load reductions have been included.

(C+D)/2 has been limited to 35 feet to correspond with the beam tables.

Column bearing design must be per the AISC Specification. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual.

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ESIDENTIAL STEEL FRAMING

+ DL is in addition to beam weight & 100plf for the intenor walls.

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Column

Beam

Tributary Area -

Tributary Width -

PLAN



Residential Steel Column Load/Spacing Tables - Pipe and Tube Columns 2&3 15 MAXIMUM COLUMN SPACING, when C = D or MAXIMUM TRIBUTARY LENGTH, (C+D)/2, when C ≠ D; ft. DL (psf) + 1st fir 15 2&3 30 LL (psf)* 40 THREE FLOORS (no roof or attic loads) - Unbraced Length of Column = 8 feet 1st fir TRIBUTARY WIDTH SUPPORTED BY THE CENTER BEAM - (A+B)/2 COLUMN **Column Properties** 22'-0 24'-0 8'-0 10'-0 12'-0 14'-0 16'-0 18'-0 20'-0 Pe Pa SIZE Weight/Ft. Fv A 5.7 5.2 7.3 6.4 ---3"dia. STD. 7.58 36 2.23 16 34 12.2 10.0 8.4 10.8 9.1 7.9 7.0 6.2 5.6 5.1 ... 13.3 2.02 35 TS 3x3x0.1875 6.87 46 17 7.2 6.5 6.0 7.9 16.8 13.7 11.6 10.0 8.8 36 22 3.5"dia. STD. 9.11 2.68 44 9.8 8.6 7.7 7.0 6.4 5.8 2.59 21 44 16.4 13.4 11.3 TS 3x3x0.2500 8.81 46 7.5 6.7 6.2 5.7 10.9 9.5 8.3 15.9 13.0 10.25 36 3.02 20 45 3"dia. X-Strg. 6.7 8.0 7.3 15.3 12.9 11.2 9.8 8.8 18.7 TS 3x3x0.3125 10.58 24 46 3.11 51 7.8 9.3 8.5 10.3 21.9 17.9 15.1 13.1 11.5 4"dia. STD. 10.79 36 3.17 28 54 10.6 9.7 8.9 20.4 17.2 14.9 13.1 11.7 25.0 TS 4x4x0.1875 9.42 2.77 32 58 46 7.9 9.4 10.4 8.6 15.3 13.2 11.7 3.5"dia. X-Strg. 3.68 29 59 22.2 18.1 12.50 36 25.9 21.9 18.9 16.7 14.9 13.5 12.3 11.3 31.8 TS 4x4x0.2500 41 75 12.21 46 3.59 10.6 12.7 11.6 17.8 15.7 14.0 29.9 24.4 20.6 4"dia. X-Strg. 14.98 36 4.41 38 75 9.9 9.1 20.8 17.6 15.2 13.4 12.0 10.8 25.5 18.58 5.47 33 77 3"dia. XX-Strg. 36 14.9 13.6 12.5 24.1 20.9 18.4 16.4 35.0 28.5 5"dia. STD. 14.62 36 4.30 45 78 14.5 13.4 25.8 22.4 19.7 17.6 15.9 35.0 30.6 TS 4x4x0.3125 14.83 46 4.36 48 90 Column loads are based on a maximum eccentricity of 1" between the resultant (total) load and the centerline of the column. Supported beams may be single span or continuous with a maximum eccentricity of 1" for the resultant load. Tributan Fy = Minimum design yield stress per the AISC Specification, ksi. K = 1.0 Area Column в A = Gross cross-sectional area of column per the AISC Manual, in. Beam Tributary Width Pe = Maximum axial load with an eccentricity of 1", per the AISC Manual, kips. Pa = Allowable axial load values from the 1989 AISC - ASD Manual, Allowable Concentric Load Tables, kips. D PLAN

* No live load reductions have been included. + DL is in addition to beam weight & 100plf for the interior walls.

(C+D)/2 has been limited to 35 feet to correspond with the beam tables.

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Column bearing design must be per the AISC Specification. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual.

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RESIDENTIAL STEEL FRAMING

June 1993

What Bible do you read? Does the bible you read make any difference?

Its no wonder people do not know what to believe with the way the Alexandrian (Egyptian) translations change the context of scripture in this chapter of Jeremiah 3

Although Most of the Alexandrian translations do not go so far as to put "The Lord says" at the beginning of verse one, they infer that it is the Lord commanding because these translations remove "They say" from the first of the verse, and with an ending of "the Lord says" at the end of the verse it seems like it is all a command of God. By removing the "They say" part a person does not know that part of what is said here is by someone other than God.

Check out this webpage :

http://marriage.as4u.us/does-the-bible-you-read-make-any-difference.html



Steel Beam and Column Tables

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MAXIMUM CO T	LUMN SP. HREE FL		5 C									L (psf) + L (psf)*	1st fir 20 1st fir 40	2&3 20 2&3 30
COLUMN		Colum	n Propert	ies			TRIBUT	ARY WID	TH SUPPO	RTED BY	THE CEN	TER BEA	M - (A+B)/2	
SIZE	Weight/Ft.	Fy	A	Pe	Pa	8'-0	10'-0	12'-0	14'-0	16'-0	18'-0	20'-0	22'-0	24'-0
3"dia. STD.	7.58	36	2.23	16	34	11.2	9.1	7.7	6.6	5.9	5.2			
TS 3x3x0.1875	6.87	46	2.02	17	35	12.1	9.9	8.3	7.2	6.3	5.7	5.1		
3.5"dia. STD.	9.11	36	2.68	22	44	15.4	12.5	10.6	9.1	8.1	7.2	6.5	5.9	5.5
TS 3x3x0.2500	8.81	46	2.59	21	44	15.0	12.2	10.3	8.9	7.8	7.0	6.3	5.8	5.3
3"dia. X-Strg.	10.25	36	3.02	20	45	14.5	11.8	10.0	8.6	7.6	6.8	6.1	5.6	5.1
TS 3x3x0.3125	10.58	46	3.11	24	51	17.1	13.9	11.8	10.2	9.0	8.0	7.2	6.6	6.1
4"dia. STD.	10.79	36	3.17	28	54	20.0	16.3	13.8	11.9	10.5	9.4	8.5	7.7	71
TS 4x4x0.1875	9.42	46	2.77	32	58	22.8	18.6	15.7	13.6	12.0	10.7	9.7	8.8	8.1
3.5"dia. X-Strg.	12.50	36	3.68	29	59	20.3	16.5	13.9	12.1	10.6	9.5	8.6	7.8	7.2
TS 4x4x0.2500	12.21	46	3.59	41	75	29.1	23.7	20.0	17.3	15.2	13.6	12.3	11.2	10.3
4"dia. X-Strg.	14.98	36	4.41	38	75	27.3	22.2	18.8	16.2	14.3	12.8	11.5	10.5	9.7
3"dia. XX-Strg.	18.58	36	5.47	33	77	23.3	19.0	16.0	13.8	12.2	10.9	9.8	9.0	8.3
5"dia. STD.	14.62	36	4.30	45	78	32.0	26.1	22.0	19.0	16.7	15.0	13.5	12.3	11.3
TS 4x4x0.3125	14.83	46	4.36	48	90	34.3	27.9	23.6	20.4	17.9	16.0	14.5	13.2	12.1
	14.83 ed on a maxin y be single sp yield stress p onal area of co oad with an e	46 num ecc an or cor er the Al elumn pe ccentricit	4.36 entricity of ntinuous wi SC Specifi er the AISC ty of 1°, per	48 1" betwee ith a max cation, ke Manual, r the AISO	90 een the re simum ec si. K = in. C Manual	34.3 esultant (tota ccentricity of 1.0 , kips.	27.9 I) load and th 1° for the res	23.6 e centerline o ultant load.	20.4	17.9	15.0 16.0	Tributary Area Tributary Width	13.2	lumn Ber

Column bearing design must be per the AISC Specification. Guidance on base plate design can be found on pages 3-106 through 3-111 of the 1989 AISC ASD Manual.

tonywmarriage@yahoo.com Subject: MARRIAGE

SIDENTIAL STEEL FRAMING

June 1993

http://WhatIsMarriage-Tw.weebly.com

METRIC CONVERSION TABLE

Quantity	From Inch-Pound Units	To Metric Units	Multiply by
Length	foot inch	m mm mm	0.304 8 304 8 25 4
Area	square foot	m²	0 092 903 04
	square inches	mm²	645 16
Force	lb	N	4.448 22
	kip	kN	4 448 22
Force/unit length	plf	N/m	14 593 9
	klf	kN/m	14 593 9
Pressure, stress, modulus	psf	Pa	47 880 3
of elasticity	ksf	kN/m	47.880 3
Bending moment, torque	ft-lb	N-m	1 355 82
moment of force	kt-kip	kN-m	1 355 82
Second moment of area	in ⁴	mm⁴	416 231
Section modulus	in³	mm ³	16 387 064



KILLING BABIES IS NO WAY TO PLAN PARENTHOOD Babies Voice Tw. Weebly.com

http://www.toolbase.org/PDF/DesignGuides/ResidentialSteelLoad_SpanTables.pdf